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MODELLING AND ANALYSIS OF SUSPENSION SYSTEM UNDER MECHANICAL LOADS

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ABST<mark>RACT</mark>

Shock absorbers are a critical part of a suspension system, connecting the vehicle to its wheels. The need for dampers arises because of the roll and pitches associated with vehicle maneuvering, and from the roughness of road. This led to make the ride quality for the people very uncomfortable which led to invention and innovation of shock absorbers. Shock absorbers are devices that smooth out an impulse experienced by a vehicle, and appropriately dissipate or absorb the kinetic energy. Shock absorbers have become such an essential component of an automobile.

In this think about, mono suspension and double suspension was considered. And alluminium alloy and stainless steel are the materials which are considered to conclude which type of suspension system gives more comfort to the rider. Comparing the ride quality of mono suspension and double suspension of two-wheeler vehicles to know how they contrast from each other by performing inactive auxiliary examination beneath diverse stacking conditions by planning 3D demonstrate of suspension framework utilizing program like CATIA V5 and ANSYS for performing examination.

INTRODUCTION

Suspension Framework:

A motorcycle's suspension serves a double reason- contributing to the vehicle's taking care of and braking and giving security and consolation by keeping the vehicle's travellers comfortably disconnected from street clamour, bumps and vibrations. Stun safeguard may be a mechanical gadget planned to smooth out or soggy stun drive and disseminate dynamic vitality. In this work, suspension framework is planned and a 3D show is made utilizing

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CATIA V5R21. Basic investigation is done on the stun safeguard by shifting distinctive sorts of materials and stacking conditions. Suspension sorts considered in this investigation are mono suspension and twin suspension frameworks. To approve the quality of the show, the auxiliary examination on the plan of suspension frameworks is performed. The investigation is done by considering diverse stacking conditions like bicycle weight, bicycle weight with single, and twofold rider. At long last, comparison is done for distinctive suspension frameworks by shifting diverse materials such as stainless steel, aluminium combination, and magnesium combination. Sorts of suspension frameworks utilized in this extend are Mono suspension and Twin suspension frameworks.

Mono Suspension framework:

Initially, Yamaha created the monoshock suspension to progress the execution of its bicycles in motocross competition. A few producers moreover utilize the term "flying suspension" for monoshock suspension. It provides a incredible bargain of soundness within the hops and arrivals of the bicycle. This suspension plan employments a single (mono) stun safeguard, greater in size. In expansion, it encompasses a more grounded spring fitted on the exterior. The monoshock is more often than not situated close the center of the bike's chassis. Besides, one of its closes connects to the chassis. In any case, the other conclusion to the raise swing- arm of the bicycle which connects to the raise wheel. As the wheel moves up or down, the monoshock safeguard either collapses or amplifies encourage. Thus, this empowers longer stroke for the stun safeguard. Hence, it comes about in longer travel for the raise wheel. Other than, this suspension is found closer to the bike's center. In this way, it makes a difference to make strides dexterity & taking care of of the bicycle.

Twin suspension framework:

Twin stun alludes to bikes that have two stun safeguards. By and large, this term is utilized to indicate a specific time of cruisers and is most regularly utilized when portraying off- street motorcycles. It is the most broadly utilized suspension in two-wheeler vehicle. It exchanges loads similarly to the chassis of the vehicle. There's not any sort of hurt to this suspension on the off chance that we increment load on the vehicle. It is broadly favored within the vehicle which is utilized in unpleasant landscape vehicle. As in unpleasant streets there's ceaselessly changing loads on the vehicle, so its suspension exchanges the load legitimately to induce superior ride consolation. The alteration of this suspension is troublesome. Ready to drive the vehicle in the event that any one of suspension gets oil spilled, harmed, and fizzled whereas driving.

DIMENSIONAL DETAILS:

Mono Suspension: Spring: Wire diameter (d)= 11mm Coil outer diameter (Do)= 46mm Coil inner diameter (Di)= 26mm Coil free height (h)= 100mm No. of active coils (n)= 5 Pitch (P)= 18mm Base: Radius= 22.5mm Shaft radius= 5mm Shaft length= 75mm

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Top part: Length= 110mm Diameter=13.5mm Inner diameter=5mm Nut: Outer diameter= 54mm Inner diameter= 24mm **Twin Suspension:** Spring: Wire diameter (d) = 7.8 mmCoil outer diameter (Do)= 68mm Coil inner diameter (Di) = 52mmCoil free height (h)= 165mm No. of active coils (n) = 8Pitch (P) = 19mm**Bottom part:** Radius= 24mm Height= 94.5mm **Top Bearing:** Base Diameter= 20mm Bearing diameter= 20mm Height = 58 mmShaft diameter= 6.5mm Length= 200mm Nut: Outer diameter= 54mm Inner diameter= 40mm Thickness= 10mm

CONSIDERATIONS:

The properties of the below considered materials aluminium alloy and stainless steel are

Aluminium Alloy:

Modulus of rigidity= 27×10^3 Mpa Modulus of elasticity= 70×10^3 Mpa Tensile yield strength= 310Mpa Compressive yield strength= 310Mpa Density= 2.7g/cm³

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Stainless steel:

Modulus of rigidity= 77.2×10^3 Mpa

Modulus of elasticity= 210×10^3 Mpa

Tensile yield strength= 505Mpa

Compressive yield strength= 505Mpa

Density= 7.83g/cm³

In this project three loading conditions are considered and they are

- 1. Weight of the bike
- 2. Weight of the bike with one person
- 3. Weight of the bike with two people

As we are working on the rear suspension systems of the bike so only 65% of the weight is considered and while considering dynamic load multiplication factor 2 is used.

Average weight of bike = 110 kg Average weight of a person = 65 kg

Mono Suspension:

1. Weight of the bike

65% of the weight of the bike= $110x\frac{65}{100}$ = 71.5kg

 $W1 = (71.5 \times 9.81) \times 2 = 1402N$

2. Weight of the bike

65% of the weight of the bike= (110+65)
$$x_{100}^{65}$$
 = 114.1kg

W2= (114.1x9.81) x2= 2238.6N

3. Weight of the bike

65% of the weight of the bike= (110+65+65) $x\frac{65}{100} = 156.7$ kg

W3 = (156.7x9.81) x2 = 3074.4N

Twin Suspension: In this suspension system the load is distributed across two shock absorbers so the actual load will be 50% of the obtained load.

1. Weight of the bike

65% of the weight of the bike= $110x\frac{65}{100}$ = 71.5kg

W1= (71.5x9.81) x2x
$$\frac{50}{100}$$
= 701N

2. Weight of the bike with one person

65% of the weight of the bike= (110+65) $x \frac{65}{100} = 114.1 \text{kg}$

W2= (114.1x9.81) x2x $\frac{50}{100}$ = 1119.3N

3. Weight of the bike with two persons

65% of the weight of the bike= (110+65+65) $x\frac{65}{100}$ = 156.7kg

W3= (156.7x9.81) $x2x\frac{50}{100}$ = 1537.2N

CALCULATIONS:

Mono Suspension (Aluminium Alloy)

Mean coil diameter(D)= $\frac{Di+Do}{2}$ = 36mm Spring index (C) = $\frac{D}{d}$ = 3.27 Wahl's stress factor (K) = $\frac{4C-1}{4C+1} + \frac{0.615}{C} = 1.51$ Maximum shear stress (τ) at W1= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 1402 \times 60}{\pi \times 11^3} = 140.02 Mpa$ Maximum shear stress (τ) at W2= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 2236.6 \times 60}{\pi \times 11^3} = 208.97 Mpa$ Maximum shear stress (τ) at W3= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 3074.4 \times 60}{\pi \times 11^3} = 286.95 Mpa$ Factor of safety at W1= $\frac{310}{140.02}$ = 2.21 Factor of safety at W2= $\frac{310}{208.97}$ = 1.48 Factor of safety at W3= $\frac{310}{286.95}$ = 1.08 Mono Suspension (Stainless steel) Mean coil diameter(D) = $\frac{Di+Do}{2}$ = $\frac{36mm}{2}$ Spring index (C) = $\frac{D}{d}$ = 3.27 Wahl's stress factor (K) = $\frac{4C-1}{4C+1} + \frac{0.615}{C} = 1.51$ Maximum shear stress (τ) at W1= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 1402 \times 60}{\pi \times 11^3} = 143.06 Mpa$ JCRI Maximum shear stress (τ) at W2= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 2236.6 \times 60}{\pi \times 11^3} = 214.57 Mpa$ Maximum shear stress (τ) at W3= $\frac{K8PD}{\pi d^3} = \frac{1.51 \times 8 \times 36 \times 3074.4 \times 60}{\pi \times 11^3} = 290.74 Mpa$ Factor of safety at W1= $\frac{505}{143.06}$ = 3.59 Factor of safety at W2= $\frac{505}{214.57}$ = 2.41 Factor of safety at W3= $\frac{505}{290.74}$ = 1.75 **Twin Suspension (Aluminium Alloy)** Mean coil diameter(D)= $\frac{Di+Do}{2}$ = 60mm Spring index (C) = $\frac{D}{d}$ = 7.69 Wahl's stress factor (K) = $\frac{4C-1}{4C+1} + \frac{0.615}{C} = 1.19$ Maximum shear stress (τ) at W1= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*701*60}{\pi*7.8^3} = 265.48 Mpa$ Maximum shear stress (τ) at W2= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*1119.3*60}{\pi*7.8^3} = 423.48 Mpa$ Maximum shear stress (τ) at W3= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*1537.2*60}{\pi * 7.8^3} = 581.59 Mpa$ Factor of safety at W1= $\frac{310}{26548}$ = 1.16

Factor of safety at W2= $\frac{310}{423.48}$ = 0.73 Factor of safety at W3= $\frac{310}{581.59}$ = 0.53 **Twin Suspension (Stainless steel)** Mean coil diameter(D)= $\frac{Di+Do}{2}$ = 60mm Spring index (C)= $\frac{D}{d}$ = 7.69 Wahl's stress factor (K)= $\frac{4C-1}{4C+1} + \frac{0.615}{C}$ = 1.19 Maximum shear stress (τ) at W1= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*682.7*60}{\pi*7.8^3} = 268.57 Mpa$ Maximum shear stress (τ) at W2= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*1044.85*60}{\pi*7.8^3} = 428.84 Mpa$ Maximum shear stress (τ) at W3= $\frac{K8PD}{\pi d^3} = \frac{1.51*8*36*1044.85*60}{\pi*7.8^3} = 588.59 Mpa$ Factor of safety at W1= $\frac{505}{268.57} = 1.84$ Factor of safety at W2= $\frac{310}{428.84} = 1.15$ Factor of safety at W3= $\frac{310}{588.59} = 0.8$

MODELLING

Modelling can be drained various methods such as wireframe demonstrating, surface modelling, solid displaying, etc. the most straightforward way is chosen for modelling. Here we have chosen strong displaying strategy of making a strong. There are many packages for displaying, out of which CATIA V5 has been chosen for its ease of accessibility and because it is client neighbourly.

Mono suspension Assembly:

Step 1: Press on Gathering plan module in mechanical plan. Right tap on item and select component and include the existing components into the get together plan.

Step 2: After adding all the components required for mono suspension framework into the get together module, press on the manipulation command and isolated each portion to put it within the redress position.

Step 3: Presently utilize imperatives instrument bar for performing required constraint operations like coincidence, off-set, contact imperative, point limitation etc.

Step 4: After performing all the limitation operations to induce the required get together, at that point at last tap on the overhaul all command to complete the get together plan. Now this assembly plan can be imported to simulation software for performing investigation.

Twin suspension Assembly:

Step 1: Tap on Assembly design module in mechanical plan. Right click on item and select component and add the existing components into the assembly design.

Step 2: After including all the components required for twin suspension system into the gathering module, press on the control command and separate each part to put it in the right position.

Step 3: Presently utilize limitations device bar for performing required imperative operations like coincidence, off-set, contact imperative, point imperative etc.

Step 4: After performing all the imperative operations to induce the required gathering, at that point at long last press on the upgrade all command to total the get together design.

After performing the theoretical calculations on both suspension systems when the suspensions are in compressed position, to support the calculations an analysis using Ansys simulation has been performed on both suspension system. The respective Maximum shear stress and factor of safety were determined and then compared.

The resultant stress obtained through calculations of suspension systems of different materials at different loading conditions are tabulated in the following table.

RESULTS

Maximum shear stress:

Mono suspension:

Type of material	Load appliedin N	Maximum shear stress (theoretical) MPa	Maximum shear stress (Ansys Simulation) MPa
Aluminium alloy			
	W1=1402N	143.06	148.6
	W2=2238.6N	214.57	210.50
	W3=3074.4N	290.74	285.44
Stainless steel			
	W1=1402N	140.02	140.36
	W2=2238.6N	208.97	209.4
	W3=3074.4N	286.74	287.68

 Table 6.1 Max. Shear stress (mono)

Twin suspension:

Type of material	Load appliedin N	Maximum shear stress (Theoretical) MPa	Maximum shear stress (Ansys Simulation)in MPa
Aluminium alloy			
	W1=701N	268.57	270.02
	W2=1119.3N	428.84	430.22
	W3=1537.2N	588.59	592.33
Stainless steel			
	W1=701N	265.22	274.35
	W2=1119.3N	423.48	438.06
	W3=1537.2N	581.59	601.61

 Table 6.2 Max. Shear stress (twin)

Factor of safety:

Mono suspension:

Type of material	Load applied in N	Factor of safety	Factor of safety
		(Theoretical)	(simulation)
Aluminium alloy			
	W1=1402N	2.213	2.33
	W2=2238.6N	1.48	1.76
	W3=3074.4N	1.08	1.35
Stainless steel			
	W1=1402N	3.59	3.66
	W2=2238.6N	2.41	2.6
	W3=3074.4N	1.75	1.88

 Table 6.3 Factor of safety (mono)

Twin suspension:

Load applied III I	Factor of safety	Factor of safety
	(Theoretical)	(Simulation)
W1=70 <mark>1N</mark>	1.16	1.3
W2=11 <mark>19.3</mark> N	0.73	1.12
W3=15 <mark>37.2N</mark>	0.53	0.98
W1=701N	1.84	2.07
W2=1119.3N	1.15	1.53
W3=1537.2N	0.83	1.12
	W1=701N W2=1119.3N W3=1537.2N W1=701N W2=1119.3N W3=1537.2N	W1=701N 1.16 W2=1119.3N 0.73 W3=1537.2N 0.53 W1=701N 1.84 W2=1119.3N 1.15 W3=1537.2N 0.83

Total deformation:

Mono Suspension:

W3=1537.2N	0.83	1.12	
Table 6.4 Factor	of safety (twin)		
			CRI
1	Cotal Deformation	in mm	
W1 = 1402 N	W2=2238.6 N	N W 3 =	3074.4 N
2.09 mm	3.12 mm	4.2	88 mm
0.761 mm	1.135 mm	1.5	59 mm
	W3=1537.2N Table 6.4 Factor W1 = 1402 N 2.09 mm 0.761 mm	W3=1537.2N 0.83 Table 6.4 Factor of safety (twin) Total Deformation W1 = 1402 N W2=2238.6 N 2.09 mm 3.12 mm 0.761 mm 1.135 mm	W3=1537.2N 0.83 1.12 Table 6.4 Factor of safety (twin) Total Deformation in mm W1 = 1402 N W2=2238.6 N W3 = 2.09 mm 3.12 mm 4.2 0.761 mm 1.135 mm 1.5

 Table 6.5 Total deformation (mono)

Twin Suspension:

Type of material	Total Deformation in mm			
	W1 = 701 N	W2=1119.3 N	W3 = 1537.2 N	
Aluminium alloy	4.99 mm	7.97 mm	10.94 mm	
Stainless steel	1.81 mm	2.90 mm	3.98 mm	

Table 6.6 Total deformation (twin)

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