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Thermal Analysis Of An Automotive Radiator Sizing And Rating— Simulation Approach

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ABSTRACT : Automotive radiator is key component of engine cooling system. Radiator thermal analysis consist sizing and rating of heat exchanger. Radiator size mainly depends on heat rejection requirement. Heat tran.sfer calculations are important fundamental.s to optimize radiator. Automotive manufacturers use 1-D simulation software to decide radiator size. This paper focuses on thermal analysis of radiator theoretically using e-NTU method and its validation by simulation approach.

Keywords - Automotive radiator, Heat transfer, Rating, Simulation, Sizing

I. INTRODUCTION

Automotive radiator is key component of engine cooling system. Coolant surrounding engine passes through radiator. In radiator coolant gets cooled down and re-circulated into system. Radiator sizing is important factor while designing cooling system. Radiator size depends on heat load as well packaging space availability. Heat load depends on heat rejection required to keep engine surface at optimum temperature. Generally LMTD or e- NTU method is used to do heat transfer calculations of radiator. Both methods have its own advantages and preferred according to data availability. When radiator inlet and outlet temperature are known LMTD gives faster solution. When any of the temperature is unknown LMTD method undergoes iterations to find solution. In this case e-NTU is better. In this paper e-NTU method is described to do heat transfer calculations.

R. HEAT TRANSFER CALCULATIONS

Purpose of thermal analysis of heat exchanger is to determine heat transfer surface area (sizing) and performance calculation to determine heat transfer rate (rating). It is necessary to find out amount of heat transfer, outlet temperatures of both duids, e-NTLJ method is based or concept of heat exchanger effectiveness.«.

[6] Here approximate size is assumed according to space availability. Based on this size heat transfer rate is calculated which should fulfill the requirement. Radiator size and heat transfer rate finalized accordingly.

Coolant side heat transfer coefficient calculations Mathematical expressions are taken from references [1,2,3,6]

- 1. Hydraulic diameter Dhc = 4*Ait/Pit
- 2. Reynolds number Rec = (Vc*Dhc)/Sc
- 3. Prandtl number Pre —(Sc*Cpe)/Kc
- 4. Nusselt number for 2300<Re<10000
- Nuc = $[(\text{Rec}-1000)*\text{Prc}*(\text{FF}/2)]/(1.07+[(12.7*(\text{FF}/2)"^{2*}(\text{Prc}"^{3}-1)]]$ where Friction factor

 $FF = [1.58*1n(Rec 3.28)]^2$

5. Heattransfer coefficient hc - (Nuc*Kc)/(Dhc)

Heat transfer coefficient air Mathematical expressions are taken from references [2,3,5,6]

- 1 Hydraulic diameter Dha— 4*Cd*Ara/Aa
- 2 Reynolds number Rea =(Vaf*Dha)/Sa
- β Prandtl number Pra= (Sa*Cpa)/Ka

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- '-I. iilU"tlI**Il Hit Jk $\mathbf{I} = \mathbf{O} \, \mathbf{174} / \mathbf{D} \, \mathbf{c} \, \mathbf{O}^{3} \, \mathbf{C}^{3}$
- $J = 0.174/Rea^{03} 8'$
- 5. Heattransfercoefficient ha =(J*Va.f*Uppa)/Pra"

Heat rejection calculations Mathematical expressions are taken from references [1,3,5,6] Factor to calculate fin efficiency F [(2*ha)/(Kt*Tht)] ⁰"*(Fh/2) 1. Temperature effectiveness of fins (fin efficiency) Ef= [TanH{F)]/F Total surface temperature 3. effectiveness of fins Eft = 1-[(1-Ef)*(Af/Aa)]Overall hermalresistance 4 Overall heat 5. transfer coefficient U = 1/R6. Sir earn ii eat sapacity ra.ie for air Ca = Ma * Cpa7. Streamheat capacityratefor coolant Cc =Mc*Cpc 8. Stream heat capacity rate ratio Cr — minimum of Ca or Cc/maximum of Ca or Cc 9. Number of transfer units CTUmax — (iJ*(Aa/2jj 'minimum ofCa or xc 10. Heat exchanger effectiveness $E - 1 - \exp\{[exp(-Cr*NTUmax^{07}) - 1]/(Cr*NTUmax^{022})\}$ 11. Tntwl bea_i irav_sfer ra.ie Q - E*minimum of Ca or Cc*(Tic-Tra) JCR Coolant Outlet Temperature 1. T oc-Tic-1. Toa = Tia + (Q/Ca)(O/Cc)Air Outlet Temperat ure

III. I-D SMULATION SOFTWARE

One-dimensional simulation software is used to designer thermal.analysis of cooling system. The cooling system is represented as a network of various parts like pipes, heat source etc. Inputs include fluid flow rates and temperatures, core dimensions, fins and tubes details like thickness, thermal conductivities, number of tubes etc. It is also possible to specify different coolant types or other system combinations or different concepts and compare them with each other. System can be analyzed at constant or variable operating conditions. Cooling system performance can be estimated independent of the vehicle measurements, earlier in development phase. Analysis accuracy can be increased by incorporating Computational Fluid Dynamics results into cooling system 1-D model design. Simulation software offers great saving in terms of cost and development time while designing cooling systems.

RADIATOR SIZING AND RATING

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Actual thermal analysis is performed first theoretically and then by simulation approach for following requirement. It includes heat rejection requirement, space available under hood to mount radiator on vehicle chas.sis. Heat transfer reo,uirement is decided a.s per engine specification, engine operating conditions and vehicle operating conditions. Cooling system design should fulfill all these requirements.

		D ·				
lable	1:	Requirement	ot	engine	cooling	system
	••		~.	+B+		

	Parameter	Unit	Value
	Total heat transfer	KW	38.93
Height	m 0	.390	
Length	m 0	.343	
Depth	m <	=0.032	

Analytical approach

Following parameters are considered for analytical approach. First radiator core size is assumed and heat transfer calculations done.

	calculations				
	Description	Parameter		Unit	Value
		Width	Cw	m	0.3423
	Core	Length	Cl	m	0.39
		Depth	Cd	m	0.032
		Density	Gf	Per m	850
	Fin	ueignt	Fn	m	u.uuS3
	1 111	Thickness	Thf	m	0.001
	1	Thermal conductivity	Kf	W/mK	200
	Tube	Rows	Ntr		1
	Volume	flotwenateal conductivity/	ı Kt	40000nK	200
	Coolant	Density	Gc	Kg/m°	1037.5
		Dynamic viscosity	Sc	kg/ms	0.001209
	Coolim	Specific heat	Срс	J/KgK	3504.97
		Thermal conductivity	Kc	W/mK	0.4375
		Inlet temperature	Tic	K	383
		Velocity	Va	mls	6
		Density	Ga	Kg/m'	1.057
	Air	Dynamic viscosity	Sa	K%ms	0.00002
		Specific heat	Сра	J/KgK	1009.95
		Thermal conducts.'ip	Ka	w 'mK	u.UUJU14
		Inlet temperature	Tra	K	323
Simulation approa	nch:	\sim		•	

Table 2: Inputs for theoretical

Cooling system modeled as shown in Fig 1 according to following parameters and steps.

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Parameter for 1-D sim		nUnit	Value
Core Width	Cw	m	0.3423
Core Length	Cl	m	0.390
More Depth	Cd	m	0.032
Fin Density	Gf	Per m	850
Number of tubes	Nt	-	42
Centaur v oiumc liuw rute	w'c	un	oñu
Coolant Inlet temperature	Tic	K	3h3
Air volume flow rate	Wa	l/s	800
Air inlet temperature	Tıa	K	323

Steps:

1.

- Heat source is selected as a radiator. Core dimensions specified.
- 2. Input and output nodes set for air and coolant inlet and outlet parameters.
- 3. Air and coolant flow direction given through network lines.
- 4. 50% / 50% water and ethylene glycol coolant is selected accordingly its thermo-physical properties like
 - ilii0v win rñvurñ, ViSiiOSivJ, uñliSiiJ TO. jirGSiilicm.
- 5. Similarly for air thermo-physical

properties given. Thermal analysis is

performed on cooling system model.

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Fig.1: 1-D simulation cooling system model

V. RESULTS AND DISCUSSION

Comparison of analytical and simulation results

Table 4: Analytical results						
Parameter		(Jnit	Vaiiie I			
Total heat transfer	Q	KW	42.368			
Coolant outlet temperature	Toc	K	374.4			
Airoutlettemperature	Toa	K	372.54			

Table 5: Simulation results

	Parameter	Unit	Value
Total hea	at transfer O KW 4	1.944	
	Coolant outlet temperature Toc	K	374.02
	Airoutlettemperature Toa	K	372.0

Comparison shows that both results closely matched with each other. Thus theoretical thermal analysis of radiator using e-NTU method is validated using simulation approach. Core dimensions are fixed from these

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FUTURE SCOPE

In broad manner simulation approach is useful tool for thermal analysis of cooling system. It is more helpful when cooling system involves more than oneheatexchanger. With thehelp of advance simulation software it is possible to analyze complete vehicle thermal management.

Nomenclature

A: Total heat transfer area Ar : Free flow area Ai:Inside crosssection area Pi: Inside perimeter Fh: Fin height G: Density Th: Thickness K : Thermal conductivity FF: Friction factor

 $E : E a amo t^{\circ} fhea_t Gahfer "$

Eft : Tidal s fac te peea e e ectiveness of fin Ef: Temperature effectiveness offin HH c 984 |

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	- J	0 -0-0 -0 0		
To : Outlet te NTU : Numb M : Ma.s.s f)o W : Volume f Specific heat U : Overall he thermal resists h : Heat trans Nu : Nusselt r n_umher Pr : H V : Velocity Vaf: Air mass Dynamic viso J : Colbum fac	emperature ber of transfer units ow rate low rate Cp : eat transfer coeffici ance sfer coefficient number Re : Reynol Prandtl number s flow velocity S : cosity ctor	:s ient R: Overall ldqs :		
Subscripts:- a: Air	c:Coolant			
t : Tube f: Fin	n			
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		V		
		PRESSURE		
OUTLET TANK	a de la companya de la	INLET		
PARTS OF C	AR RADIATOR			
	Name of	radiator parts		
	1.Toptank			

- 2 Bottom tank 3 Fan
- 4 Radiator core
- 5 Cooling Fins
- 6 Pressurecap

7Filler neck

8 Expention tank