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# ANALYSIS OF SHEAR WALL FRAMED BUILDING FOR DIFFERENT LOCATION UNDER SEISMIC CONDITION

<sup>1</sup> Mohan Kanojiya, <sup>2</sup>Vaibhav Assudani, <sup>3</sup>Anchal Rahate, <sup>4</sup>Nazeef Afzal, <sup>5</sup>Prof. Sayyed Aamir Hussain

<sup>1</sup>UG Student, <sup>2</sup>UG Student, <sup>3</sup>UG Student, <sup>4</sup>UG Student, <sup>5</sup>Professor <sup>1</sup>Department of Civil Engineering,

<sup>1</sup> Anjuman College of Engineering & Technology, Nagpur, India

*Abstract:* In seismic design of multistoried building, shear walls are most common structure adopted to make the structure earthquake resistant. These are constructed to counteract the lateral loads caused by wind load and seismic loads. Shear walls provide adequate stiffness to the structure. So that the lateral drift will be in limits. Generally shear walls are the vertical cantilever which acts as a column. This investigation presents the study and comparison of earthquake behaviour of buildings with and without shear wall using STAAD Pro. In this study, reinforced concrete buildings are analyzed by changing the various position of shear wall with different locations considering various parameters such as story drift, lateral displacement and others.

#### Index Terms - Seismic analysis, Shear wall, Story drift, STAAD Pro V8i.

#### I. INTRODUCTION

Now-a-days multistoried buildings are rapidly constructed everywhere in the world and they are more slender and more sway than earlier buildings. The deformation of tall structures is composed of axial, bending, torsion, transverse shear. In recent period many new concepts and methods are adopted in field of seismic design. In general, RCC structures are constructed to control the lateral displacement. Shear walls are most common structural system which provides lateral stiffness and stability against the lateral loads. In frame structure, the shear walls behaviour is similar to the column which is subjected to combined flexure and axial load. So these are also called flexural members. Shear walls require proper designing and detailing in high seismic regions. Therefore it is necessary to determine the efficient, effective and ideal location of shear wall. This paper represents the analysis of structure with the effect of shear wall position on lateral displacement and story drift in RC frames. The analysis of shear wall was performed by STAAD Pro V8i using surface elements.

#### **II. LITERATURE REVIEW**

Shear wall system is most significantly used for tall structure in earthquake prone area. So, there are many research work was done in various aspects of shear walls which are as follows:

P.P. Chandurkar et.al. (2013) presented a study on "seismic analysis of RCC building with and without shear wall". The paper determined the lateral displacement, story drift ratio, concrete quantity, total cost, % of Ast in column required of tenth storied building calculated by placing the shear wall in different location. From that analysis, the building with shear in short span at corner (model 4) is economical as compared to others.

Wakchaure M.R et.al.(2012) presented a study on "earthquake analysis of high rise building with and without infill walls". In this analysis G+9, RCC frame building with the effect of masonry infill wall was studied. The top story displacement of high rise building reduces due to infill walls.

K.LovaRaju et.al.(2015) studied the effective location of shear wall on performance of building frame subjected to earthquake load. The pushover analysis for various models observed the structure with appropriate placed of shear wall has more significant of displacement and base shear

#### **III. BUILDING MODELLING**

In the present study, a RCC G+10 storied residential building with 3 meters height for each story is modeled. This residential building is designed as a plan of 24 x 30 m with a lift at centre. M25 grade of concrete and Fe 500 structural steel is used. The structure is supported as fixed at its base. The buildings are modeled and analyzed by using the software STAAD Pro V8i. Models are studied four zone IV comparing story drift, maximum lateral displacement etc. The study of models is designed by placing the shear wall in different location with the thickness of 250mm.

Model 1- BARE FRAME

Model 2- POSITION 'A'

Model 3- POSITION 'B'

Model 4- POSITION 'C'

Model 5- POSITION 'D'

#### **3.1 Physical Details**

The preliminary data taken for the analysis is as follows:- All the dimensions in mm. • No of stories: G+10

- Storey height: 3 m
- Beam size in all direction: 300 x 500 mm2
- Column size: 400 x 500 mm2
- Thickness of the slab:150mm
- Grade of concrete: M25
- Grade of steel: Fe500
- Density of concrete: 25 KN/m3
- Density of brick: 20 KN/m3

#### **3.2 Building Plans**



#### Fig 1:- Plan of Bare Frame Building





Fig 2:- Plan of Shear Wall At Position 'A'



Fig 4:- Plan of Shear Wall At Position 'C'

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Fig 5:- Plan of Shear Wall At Position 'D'

#### Methodology

The loading of building is subjected to dead load and live load as per IS 875 (Part 1) (Part 2): 1987 respectively. As per Indian Code of Practice IS 1893 (Part 1): 2016, design the multistoried residential building against earthquake and wind loads. The member forces are calculated with load combination given in IS 456: 2000. Seismic provision for this building:

- Seismic zone : IV
- Types of the frame : Special Moment Resisting Frame
- Response reduction factor (R) : 5.0
- Importance factor (I) : 1.2
- Soil type : Medium soil
- Damping ratio : 5%

## LOAD CASES & COMIBATIONS

ы	JAD	CASE	DESCR	IP I	IUN		
1	EQX	K+	Seismic	in X	K +ve dire	ction	
2	EQX	K- Se	eismic in X -ve o	lire	ction		
3	EQZ	Ζ+	Seismic	in Z	2 +ve direc	ction	
4	EQZ	<u>Z</u> -	Seismic	in Z	-ve direc	tion	
5	D.L		Dead Lo	ad			
6	L.L		Imposed	Lo	ad		
7	RSX	K	Response	e sp	ectrum in	X dire	ection
8	<b>RSZ</b>		Response	e sp	ectrum in	Z dire	ection
			-	-			

#### NO. LOAD COMBINATIONS

- 9 D.L+L.L 10 1.5(D.L+L.L) 11 1.2 (D.L+L.L+EQ X+ 1.2 (D.L+L.L+EQX-) 12 13 1.2 (D.L+L.L+EQZ+) 14 1.2 (D.L+L.L+EQZ-) 15 1.5 (D.L+EQX+)16 1.5 (D.L+EQX-) 1.5 (D.L+EQZ+) 17 1.5 (D.L+EQZ-) 18 19 0.9 D.L + 1.5 EQ X+ 20 0.9 D.L + 1.5 EQ X-21 0.9 D.L + 1.5 EQ Z+ 22 0.9 D.L + 1.5 EQ Z-23 D.L+0.8LL+0.8EQX
- 24 D.L+0.8LL-0.8EQX
- 25 D.L+0.8LL+0.8EQZ
- 26 D.L+0.8LL-0.8EQZ
- 27 D.L+EQX
- 28 D.L-EQX
- 29 D.L+EQZ
- 30 D.L-EQZ
- 31 D.L+0.25LL



### IV. ANALYSIS AND RESULT

The structural analysis of all models with and without shear walls have been done by using STAAD Pro. The comparison of different parameters such as maximum lateral displacement, story drift and other parameters are studied.

### 1. BASE SHEAR CRITERA

Frame Type	Load Case	Storey	Levels	Max. Sto Shear in direction	Max. Storey Shear in Z direction
Bare Frame	RSX	Base	-3.00	3589.04	3589.32
А	RSX	Base	-3.00	3752.05	3771.39
В	RSX	Base	-3.00	3954.24	4261.90
С	RSX	Base	-3.00	4294.04	4268.96
D	RSX	Base	-3.00	4849.38	5064.36

POSITION 'B' 'C'& 'D' ARE EFFECTIVE IN DEFLECTION CRITERIA



Fig 6:- Graph for Maximum Base Shear

2. DEFLECTION CRITERA

	DISPLACEMENT VALUES BY STAAD PRO											
S.No.	Frame type	Total building height	Node No.	Load Combination	Max. Displacement in 'X' Direction	Max. Displacement in 'Z' Direction	Max. permissible displacement allowed - H/500	Check for X direction	Check for Z direction			
		(m)		(L/C)	(mm)	(mm)	(mm)					
1	Bare Frame	33	625	DL+EQ	66.38	62.39	66	NOT OK	ок			
2	Α	33	625	DL+EQ	34.24	27.73	66	OK	OK			
3	В	33	625	DL+EQ	27.27	29.15	66	OK	OK			
4	С	33	625	DL+EQ	37.11	31.04	66	OK	OK			
5	D	33	627	DL+EQ	30.55	21.49	66	OK	OK			
POSITI	ON 'B' &	'D' ARE	EFFECT	IVE IN DEF	LECTION CRI	FERIA						



Fig 7:- Graph for Maximum Displacement



Fig 8: Deflection In Building

## 3. STOREY DRIFT CRITERA

STOREY DRIFT CALCULATIONS											
S.No.	Frame Type	Node No.	Load Combination	Max. Displacemen t in 'X' Direction (dx)	Max. Displacemen t in 'Z' Direction (dz)	Floor to Floor Height	Storey drift (Dx)	Storey drift (Dz)	Storey drift limitation (0.004H)	Check for X direction	Check for Z direction
		(m)	(L/C)	(mm)	(mm)	(m)	(mm)	(mm)	(mm)		
		20	DL+EQ	4.89	4.08	3.00	4.89	4.08	12	ок	ок
		120	DL+EQ	11.89	10.62	3.00	7.00	6.54	12	ок	ок
		169	DL+EQ	19.11	17.55	3.00	7.22	6.93	12	ОК	ОК
		218	DL+EQ	26.31	24.47	3.00	7.20	6.92	12	ОК	OK
		267	DL+EQ	33.37	31.24	3.00	7.06	6.77	12	ОК	OK
1	Bare	316	DL+EQ	40.18	37.74	3.00	6.81	6.50	12	ОК	OK
1 1	Frame	365	DL+EQ	46.59	43.85	3.00	6.41	6.11	12	ОК	OK
		414	DL+EQ	52.44	49.39	3.00	5.85	5.54	12	ОК	OK
		463	DL+EQ	57.55	54.20	3.00	5.11	4.81	12	ОК	OK
		512	DL+EQ	61.70	58.08	3.00	4.15	3.88	12	ОК	OK
		561	DL+EQ	64.68	60.83	3.00	2.98	2.75	12	ок	OK
		610	DL+EQ	66.38	62.39	3.00	1.70	1.56	12	ОК	OK
		37	DL+EQ	0.91	0.70	3.00	0.91	0.70	12	ок	OK
		135	DL+EQ	2.67	2.04	3.00	1.76	1.34	12	ОК	OK
		184	DL+EQ	5.04	3.86	3.00	2.37	1.82	12	ок	OK
		233	DL+EQ	7.87	6.06	3.00	2.83	2.20	12	ОК	ОК
		282	DL+EQ	11.00	8.52	3.00	3.13	2.46	12	ОК	ОК
2		331	DL+EQ	14.31	11.16	3.00	3.31	2.64	12	ОК	OK
<sup>2</sup>		380	DL+EQ	17.71	13.90	3.00	3.40	2.74	12	ОК	OK
		429	DL+EQ	21.09	16.66	3.00	3.38	2.76	12	ок	ОК
		478	DL+EQ	24.38	19.39	3.00	3.29	2.73	12	ок	OK
		527	DL+EQ	27.53	22.04	3.00	3.15	2.65	12	ОК	OK
		576	DL+EQ	30.50	24.57	3.00	2.97	2.53	12	ок	ок
		625	DL+EQ	33.28	26.96	3.00	2.78	2.39	12	ок	ОК

	STOREY DRIFT CALCULATIONS										
				Max.	Max.						
	Frame		Load	Displacemen	Displacemen	Floor to	Storev	Storev	Storey drift	Check for X	Check for Z
S.No.	Туре	Node No.	Combination	t in 'X'	t in 'Z'	Floor	drift (Dx)	drift (Dz)	limitation	direction	direction
	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			Direction	Direction	Height		(	(0.004H)		
				(dx)	(dz)						
		(m)	(L/C)	(mm)	(mm)	(m)	(mm)	(mm)	(mm)		
		3/	DL+EQ	0.77	0.58	3.00	0.77	0.58	12	OK	
		135	DL+EQ	2.15	1.60	3.00	1.38	1.02	12		OK
		104	DL+EQ	3.99	2.95	3.00	1.84	1.35	12		
		233		0.19	4.57	3.00	2.20	1.02	12		
		331	DL+EQ	11.24	8.33	3.00	2.45	1.01	12	OK	
3	В	380	DI +FQ	13.93	10.35	3.00	2.00	2.03	12	OK	OK
		429	DL+EQ	16.62	12.42	3.00	2.69	2.06	12	OK	OK
		478	DL+EQ	19.27	14.45	3.00	2.65	2.03	12	ОК	ок
		527	DL+EQ	21.82	16.44	3.00	2.55	1.99	12	ОК	ОК
		576	DL+EQ	24.24	18.34	3.00	2.42	1.90	12	ОК	ОК
		625	DL+EQ	26.50	20.14	3.00	2.26	1.80	12	ОК	ОК
		37	DL+EQ	1.02	0.78	3.00	1.02	0.78	12	OK	OK
		135	DL+EQ	3.06	2.36	3.00	2.04	1.58	12	OK	OK
		184	DL+EQ	5.83	4.52	3.00	2.77	2.16	12	OK	
		233		9.10	/.11	3.00	3.27	2.59	12		
		331		12.07	9.90	3.00	2.71	2.0/	12		
4	C	380	DL+EQ	20.11	16.12	3.00	3.73	3.10	12	OK	
		429	DL+EQ	23.73	19.12	3.00	3.62	3.07	12	OK	OK
		478	DL+EQ	27.18	22.17	3.00	3.45	2.98	12	ОК	ок
		527	DL+EQ	30.39	25.01	3.00	3.21	2.84	12	OK	OK
		576	DL+EQ	33.34	27.68	3.00	2.95	2.67	12	ОК	ОК
		625	DL+EQ	36.04	30.16	3.00	2.70	2.48	12	ОК	ОК
				STORE	Y DRIFT C		TIONS				
				Max.	Max.						
C No.	Frame	Node No.	Load Combination	Displacemen	Displacement	Floor to	Storey	Storey	Storey drift	Check for X	Check for Z
3.140.	Туре			in 'X'	in 'Z'	Height	drift (Dx)	drift (Dz)	0 004H)	direction	direction
<u> </u>			1	Direction (dx)	Direction (dz)	rieigne			(0.00111)		
					· · · · ·						
	 Para	(m)	(L/C)	(mm)	(mm)	(m)	(mm)	(mm)	(mm)		
1	Bare Frame	(m) 20	(L/C) DL+EQ	(mm) 4.89	(mm) 4.08	(m) 3.00	(mm) 4.89	(mm) 4.08	(mm) 12	 ОК	 ОК
1	Bare Frame	(m) 20	(L/C) DL+EQ	(mm) 4.89	(mm) 4.08	(m) 3.00	(mm) 4.89	(mm) 4.08	(mm) 12	 ОК	 ок
1	Bare Frame	(m) 20 39	(L/C) DL+EQ DL+EQ	(mm) 4.89 0.80	(mm) 4.08 0.58	(m) 3.00 3.00	(mm) 4.89 0.80	(mm) 4.08 0.58	(mm) 12 12	 ОК ОК	 ОК ОК
1	Bare Frame	(m) 20 39 137	(L/C) DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27	(mm) 4.08 0.58 1.60	(m) 3.00 3.00 3.00	(mm) 4.89 0.80 1.47	(mm) 4.08 0.58 1.02	(mm) 12 12 12 12	 ОК ОК ОК	 ОК ОК ОК
1	Bare Frame	(m) 20 39 137 186	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25	(mm) 4.08 0.58 1.60 2.96	(m) 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98	(mm) 4.08 0.58 1.02 1.36	(mm) 12 12 12 12 12 12	 ОК ОК ОК ОК	 ОК ОК ОК
1	Bare Frame	(m) 20 39 137 186 235	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63	(mm) 4.08 0.58 1.60 2.96 4.58	(m) 3.00 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98 2.38	(mm) 4.08 0.58 1.02 1.36 1.62	(mm) 12 12 12 12 12 12 12	 ОК ОК ОК ОК	 OK OK OK OK
1	Bare Frame	(m) 20 39 137 186 235 284 232	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 9.28	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87	(mm) 4.08 0.58 1.02 1.36 1.62 1.82	(mm) 12 12 12 12 12 12 12 12 12	 ОК ОК ОК ОК	 OK OK OK OK OK
1	Bare Frame	(m) 20 39 137 186 235 284 333 382	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87 2.98	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.96 2.04	(mm) 12 12 12 12 12 12 12 12 12 12 12	 ОК ОК ОК ОК ОК	 ОК ОК ОК ОК ОК
5	Bare Frame	(m) 20 39 137 186 235 284 333 382 431	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87 2.98 3.01	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.82 1.96 2.04 2.06	(mm) 12 12 12 12 12 12 12 12 12 12 12 12	 ОК ОК ОК ОК ОК ОК ОК	 OK OK OK OK OK OK
5	Bare Frame	(m) 20 39 137 186 235 284 333 382 431 480	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15	(mm) 4.08 0.58 1.80 2.96 4.58 6.40 8.36 10.40 12.46 14.51	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	(mm) 4.89 0.80 1.47 1.98 2.38 2.88 2.87 2.98 3.01 2.98	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.96 2.04 2.06 2.05	(mm) 12 12 12 12 12 12 12 12 12 12 12 12 12	 ОК ОК ОК ОК ОК ОК ОК	 OK OK OK OK OK OK OK
5	Bare Frame	(m) 20 39 137 186 235 284 333 382 431 480 529	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 16.51	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87 2.98 2.87 2.98 3.01 2.98 2.89	(mm) 4.08 0.58 1.02 1.38 1.62 1.82 1.96 2.04 2.06 2.05 2.00	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK
5	Bare Frame	(m) 20 39 137 186 235 284 333 382 431 480 529 578	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04 26.82	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 16.51 18.42	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98 2.38 2.88 2.87 2.98 3.01 2.98 2.89 2.89 2.78	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.96 2.04 2.06 2.00 1.91	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK OK
5	Bare Frame	(m) 20 39 137 186 235 284 333 382 431 480 529 578 627	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04 26.82 29.43	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 18.51 18.51 18.42 20.22	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98 2.38 2.87 2.98 3.01 2.98 3.01 2.98 2.89 2.78 2.81	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.96 2.04 2.06 2.05 2.00 1.91 1.80	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK OK OK
1	Bare Frame D	(m) 20 39 137 186 235 284 333 382 431 480 529 578 627 & 'D' AR	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ EFFECTIVE	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04 26.82 29.43 E IN DEFLE	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 18.51 18.51 18.42 20.22 CTION CR	(m) 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	(mm) 4.89 0.80 1.47 1.98 2.38 2.87 2.98 3.01 2.98 3.01 2.98 2.89 2.78 2.61	(mm) 4.08 0.58 1.02 1.36 1.62 1.82 1.96 2.04 2.06 2.05 2.00 1.91 1.80	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK OK OK
1	Bare Frame D	(m) 20 39 137 186 235 284 333 382 431 480 529 578 627 & 'D' AR	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ EFFECTIVE	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04 26.82 29.43 E IN DEFLE	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 18.51 18.42 20.22 CTION CR	(m) 3.00 3	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87 2.98 3.01 2.98 3.01 2.98 2.89 2.78 2.61	(mm) 4.08 0.58 1.02 1.38 1.62 1.82 1.96 2.04 2.06 2.05 2.00 1.91 1.80	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK OK OK
1	D Fion 'B'	(m) 20 39 137 186 235 284 333 382 431 480 529 578 627 & 'D' AR	(L/C) DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ DL+EQ EFFECTIVE	(mm) 4.89 0.80 2.27 4.25 6.63 9.31 12.18 15.16 18.17 21.15 24.04 26.82 29.43 EIN DEFLE	(mm) 4.08 0.58 1.60 2.96 4.58 6.40 8.36 10.40 12.46 14.51 18.42 20.22 CTION CR	(m) 3.00 3	(mm) 4.89 0.80 1.47 1.98 2.38 2.68 2.87 2.98 3.01 2.98 2.89 2.78 2.78 2.61	(mm) 4.08 0.58 1.02 1.38 1.62 1.82 1.96 2.04 2.06 2.05 2.00 1.91 1.80	(mm) 12 12 12 12 12 12 12 12 12 12	 OK OK OK OK OK OK OK OK OK OK	 OK OK OK OK OK OK OK OK OK
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Fig 9: Graph for Maximum Storey Drift

#### 4. FUNDAMENTAL NATURAL PERIOD CRITERA

MODE	Maximum Fundamental Natural Period (T) in sec.									
	Bare Frame	A	В	С	D					
1	2.245	1.452	1.292	1.533	1.341					
2	2.175	1.296	1.120	1.384	1.123					
3	2.038	0.904	0.842	1.076	0.872					
4	0.738	0.383	0.339	0.419	0.344					
5	0.711	0.329	0.289	0.362	0.290					
6	0.670	0.219	0.212	0.274	0.215					
7	0.428	0.200	0.197	0.198	0.198					
8	0.409	0.188	0.186	0.196	0.188					
9	0.391	0.186	0.180	0.186	0.181					
10	0.298	0.179	0.173	0.181	0.174					
11	0.280	0.174	0.172	0.171	0.173					
12	0.271	0.172	0.163	0.170	0.163					
13	0.225	0.168	0.160	0.167	0.161					
14	0.207	0.161	0.160	0.160	0.161					
15	0.203	0.160	0.160	0.158	0.159					
DOCITION (D) 0										

POSITION 'B' & 'D' ARE EFFECTIVE IN DEFLECTION CRITERIA



Fig 10: Graph for Maximum Natural Period

#### V. CONCLUSION

- From the comparison of the result it is found that the effective location of shear wall is found in the corner of the building.
- It can be concluded the provision of the shear wall decrease the time period comparatively with the bare frame.
- To provide shear wall increase the seismic performance of the structure.
- Tested model are A,B,C,D &Bare frame ( without shear wall ). In this tested models we observed that two of them B & D are effectively resist the criteria story drift than bare frame.

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